A NEW NAME! As a result of the merger of the Naval Ordnance Laboratory, White Oak, Maryland and the Naval Weapons Laboratory, Dahlgren, Virginia, we have a new name:







NAVAL SURFACE

NAVAL ORDNANCE LABORATORY, WHITE OAK, MD.

A950308

Photographs showing the unique mechanical memory upon the application of heat (courtesy of Goodyear Aerospace Corporation)

\*Name derived from Ni-Ti-NOL. Prefix numerical value (e.g., 55-Nitinol) indicates the nickel content in weight percent. The balance is titanium.

BASED ON THE TITANIUM-NICKEL COMPOUND TINI

# 55 MITINOL

- **■** Unique Mechanical Memory
- Mechanical Vibration Damping
- Non-Magnetic

- Corrosion Resista
- Lower Density

Accession for

NTTS
Description

Outside Accession for

Unannoused

Cutting ation

By

Distribution

Availability Codes

Availability Codes

Special

### PHYSICAL PROPERTIES

and the second of the second o	UIV	U 1 11 - 11		
Density Melting Point	6.45 g/cm³ 0.234#/in 1310°C 2390°F	3		
Magnetic Permeability -	< 1.002			
Mean Coef. of Thermal Expansions(24* – 900°C); √(x 10-6)	10.4/°C 5.8/°F			
Electrical Resistivity	Ref: 16			
Specific Heat	Ref. 17			
and the second section of the second second	the many of the party of the second	. *		

### TENSILE PROPERTIES

***	ÜLTIMATE TENSILE STRENGTH (psi)	YIÈLD STRENGTH AT 0/2% OFFSET (psi)	TOTAL ELONGATION (%)		YOUNG'S MODULUS (psi x 104)	SHEAR: MODULUS (psi x 10°)	POISSON'S RATIO
Annealed* Cold Deformed	125,000 up to 222,000	24,000 up to 61,000	60 15 (min)	20	10.2 10.2	3.6 4.0	0.33 0.28

<sup>\*</sup>Data obtained on hot wrought alloys employing 2-inch gage lengths

# MECHANICAL MEMORY PROPERTY

55-Nitinol plastically deformed below its critical temperature (A<sub>s</sub>) will recover its original shape when heated above its critical temperature. THIS PHENOMENA IS ILLUSTRATED ON THE COVER OF THIS BROCHURE. The critical transition temperature for recovery varies from -10°C to 100°C as a function of Ni:Ti ratio around the stoichiometric TiNi composition. Transition temperatures in the cryogenic range are also possible by partial substitution of cobalt for nickel. The range of recovery is controlled by mass and processing variables and may be held readily within a 10°C spread.

# DAMPING PROPERTY

The specific damping capacity of 55-Nitinol is about 25 percent when measured at a stress level of 5000 lbs/in². This is about three times the damping capacity of gray cast iron (8%). Specific damping capacity is the percentage of vibration energy absorbed per cycle. A more complete description of Nitinol and other high damping materials is given in Reference 11.

## **FABRICATION**

#### **WORKING CHARACTERISTICS:**

May be hot worked directly from the arc-melted ingot employing conventional tools, e.g., rolling, forging, swaging, etc. Recommended hot working temperature range 700° to 900° C. Room temperature working is possible with intermediate anneals at or below 800° C.

### **MACHINING**

The Nitinol alloys are most satisfactorily machined with carbide tools using moderate speeds, light feeds and highly chlorinated cutting oil. Grinding, employing silicon carbide wheels, has been found to be highly satisfactory. By careful control of the grinding conditions very fine finishes are possible. A more complete guide to the machining of the Nitinol alloys is given in Reference 3 at the end of this Data Sheet.

### MARINE CORROSION PROPERTIES:

#### STRESS-CORROSION:

Employing the U.S. Naval Research Laboratory testing method, 55-Nitinol showed no susceptibility to stress corrosion failure. 55-Nitinol, in both the annealed and the cold worked condition tested at stresses up to 100% of the yield strength exhibited no crack propagation in a sea-water environment.

#### HIGH-VELOCITY MARINE CONDITIONS:

The 55-Nitinol alloy exhibited superior resistance to erosion by high velocity sea water. Sixty day jet impingement at 15 ft/sec. sea water and 30 day cavitation tests at 117 ft/sec. resulted in negligible erosion of this alloy.

# POTENTIAL APPLICATIONS

and the second substitution of different substitution and the second substitution and second substitut	PROPERTY						
APPLICATION.	NON-MAGNETIC	LOWER DENSITY	CORROSION RESISTANCE	VIR: TION DAILPING	LOW TEMPERATURE TOUGHNESS	MFCHANICAL MEMORY	
Noise and Vibration Reducing Components		*					
Temperature Sensing Devices	***	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	**************************************			<b>X</b>	
Outer Space and Hydrospace Erectable Structures	* <b>X</b>	XX X	<b>X</b>			<b>X</b>	
Cryogenic Equipment		×	×	3	X		

# HARDNESS .

1,	CONDITION	ا و ا	RO	CKWĘLĻ 🛁	
0	Wrought (as received) After Rolling at 950° C		0 - 7	4 RC	Ø
7	1000°C Furnace Cool 1000°C Water Quench		9 1) 8	ORB 9 RB	

## **IMPACT PROPERTIES**

	TESTING	IMPACT STRENGTH (H-lb)			
COMPOSITION	TEMPERATURE (°C).	UNNOTCHED	NOTCHED		
55 Nitinol	Room	117	24		
55.1 Nitiriol (0:08 Fe)	Room -80	155 160	Variation of the state of the s		

Hot wrought material was used to produce standard Charpy impact specimens. Applications for Nitinol should follow normal design practice for notch sensitive materials.

### **FATIGUE PROPERTIES**

STRESS (psi) 70,000

CYCLES:

REMARKS No failure

Standard Rotating Beam (R. R. Moore) Test.

# REFERENCES: Design and Engineering

- 1. "Nitinols Are Non-magnetic, Corrosion Resistant, Hardenable," Materials in Design Engineering, pg. 82, Feb. 1962.
- 2. "TiNi-Ductile Intermetallic Compound," Transactions Quarterly ASM, Vol. 55, No. 2, pg. 269, June 1962.
- 3. "Machinability of Nickel-Titanium Alloys," Metcut Research Associates, Inc., Cincinnati, Ohio, Metcut Report No. 573-4062-1, June 1963. Available from Office of Technical Services, U. S. Dept. of Commerce as Report No. AD-419009, 1964.
- 4. "Growth of TiNi Single Crystals by a Modified Strain Anneal Technique," J. Appl. Phys., Vol. 35, No. 12, pg. 3620, December 1964.
- 5. "Tensile Properties of NiAl and NiTi", Journal Institute of Metals (London) Vol. 94, pg. 169; 1966.
- 6. "Effect of Addition of Oxygen, Nitrogen, and Hydrogen on Microstructure and Hardness of Cast TiNi Intermetallic Compound," ASM Transactions Quarterly, Vol. 58, No. 3, pg. 415, Sept. 1965.
- 7. "Effects of Alloying upon Certain Properties of 55.1 Nitinol." NOL Technical Report 64:235, May 1965.
- 8. "Effect of Cold Work on Room Temperature Tensile Properties of TiNi Intermetallic Compound," ASM Transactions Quarterly, Vol. 59, No. 2, pg. 350, June 1966.
- 9. "Study of Transition Element/Intermetallic Compounds," The 9th Navy Science Symposium, ONR; in press.

- 10. "The Mechanical Properties as a Function of Temperature and Free Electron Concentration in <u>Stoichiometric TiNi</u>, TiCo and TiFe Alloys." Proceedings of the First International Conference on Fracture, (Sendai, Japan), Vol. 2, Sept. 1965.
- 11. "HIDAMETS—Motals to Reduce Noise and Vibration;" The Engineer, August 5, 1966.
- 12. "Nickel-Titanium Alloys, Low Magnetic Effects; Bars, Plates, Sheets, Strips and Shapes (For Special Purpose Tools and Equipment)." Mil-N-81191 (WP) 18 December 1964.

# REFERENCES: Fundamental Theory

- 13 "Martensitic Transformations in the TiNi Compound," Proceedings 5th International Symposium on the Reactivity of Solids (Munich, Germany), Elsevier Publishing Co., Aug. 1964.
- 14. "The Thermal Conductivity, Thermoelectric Power, and the Electrical Resistivity of Stoichiometric TiNi in the 3 to 300° K Temperature Range," Journal of Applied Physics, Vol. 35, No. 10, pg. 2919, Oct. 1964.
- 15. "Crystal Structure and a Unique 'Martensitic' Transition of TiNi," Journal of Applied Physics, Vol. 36, No. 10, pg. 3232, Oct. 1965.
- 16. "The 60°C Irreversible Critical Range in the TiNi Transition," to be published.
- 17. "Anomalous Heat Capacity of TiNi," to be published.
- 18. "TiNi and Associated Compounds," Symposium at Naval Ordnance Laboratory, April 3-4, 1967.

